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# Comparative Study of Thyristor vs IGBT Based AC-DC Power Converter

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***Abstract*- This paper presents a comparative study of the application of Thyristor versus IGBT in AC-DC controlled power converter. Both simulation and practical experiment have been carried out to test the relationship between the average output voltage ($V_{dc}$) with firing angle (α, for Thyristor) and triggering pulse width (δ, for IGBT). Also the total harmonic distortion (THD) has been observed in both the cases. It is observed that IGBT based power converter introduces more harmonics in the system, in spite of more symmetrical output voltage wave shape.**

***Keywords— AC-DC converter, firing pulse, micro-controller, MATLAB/Simulink, Total Harmonic Distortion (THD)***

## I. INTRODUCTION

The demand for control of electric power for electric motor drive systems and industrial controls existed for many years, and this lead to early development of the Ward-Leonard system to obtain a variable dc voltage for the control of dc motor drives [1]-[4]. Different types of power converter contribute to control the electric power from one form to another. Among these converters AC-DC converter or rectifier [5]-[11] is the one which control the AC power as input and produces constant DC in the output. Modern power converters use power electronics devices which are primarily based on the switching of the power semiconductor devices [12]. The development of microprocessors [13]-[15] and microcomputer technology has a great impact on the control and synthesizing of these devices.

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Power conversion [16] from one form to another is required in case of the control of the electric power and the switching capability of the power devices permit these conversions. The most recent advancement in the power electronic circuits is the IGBT [17] due to its faster switching speed and lower switching and conduction losses having the three terminals: gate, collector and emitter. The most challenging task in a power conversion circuit is the development of control circuit [18]-[20]. Control circuit mainly depends on firing pulse. Firing pulse circuit can be two types, digital and analog. Analog circuit consist of electronic components which makes the circuit big in size and more complex. On the other hand, digitally controlled circuit such as microcontroller based firing pulse generation circuit become so much popular day by day because of its user friendly automatic controlling system and the circuit robustness.

It is observed that most of the researcher reported work on thyristor only. In the proposed work a microcontroller based firing circuit for single phase half-wave AC-DC converter will be implemented using both thyristor and IGBT in an integrated circuit and then performance will be evaluated with resistive load. In consequence the switching response will be fast and the switching loss would be minimized.

## II. CONTROLLED RECTIFIER

### A. Silicon Controlled Rectifier (SCR or Thyristor)

Controlled rectifiers are line commutated ac to dc power converters [21]-[22] which are used to convert a fixed voltage, fixed frequency ac power supply into variable DC output voltage.

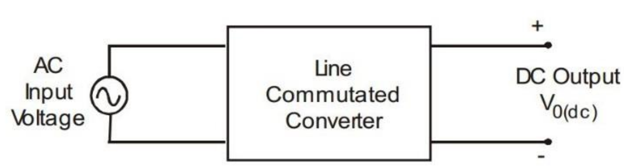


Fig. 1. Block diagram of AC-DC Converter

Fig. 1. shows the basic block diagram of ac-dc converter where the ac supply is fed to a controlled rectifier at a fixed rms voltage and at a fixed frequency. By employing phase controlled thyristor [23]-[25] in the controlled rectifier circuits variable dc output voltage and variable dc output current can be obtained by varying the firing angle (phase angle) [26]. The

basic operation principle of single phase half wave ac-dc converter is shown in the Fig. 2. When the thyristor is fired at a firing angle of $\omega t = \alpha$, the thyristor conducts from $\omega t = \alpha$ to $\pi$ radians. For a purely resistive load, the load current *Io* (output current) that flows when the thyristor is ON, is given by the expression (1). The output load current waveform is in phase to the output load voltage waveform during the thyristor conduction time from α to π.

$$i_0 = \frac{v_0}{R_L}\ , \ \text{for } \alpha \leq \omega t \leq \pi \qquad (1)$$

The firing angle α is measured from the beginning of each positive half cycle to the time instant when the gate firing pulse is applied. The input and output voltage wave shape of thyristor controlled ac-dc converter is shown in Fig. 3.

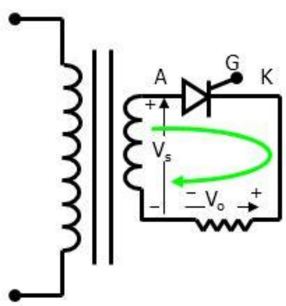


Fig. 2. Single phase half -wave thyristor controlled rectifier with resistive load

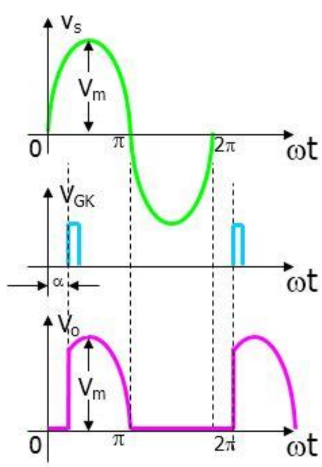


Fig. 3. Input and output voltage waveforms of single phase half-wave controlled rectifier with resistive load

The average dc output voltage is given by the expression (2) [27]

$$V_{dc} = \frac{V_m}{2\pi}\ [\, 1 + cos\alpha \,] \qquad (2)$$

The relationship between average output voltage with firing angle is represented graphically in Fig. 4 where average output voltage maximum and minimum when the value of α is $0^0$ and $180^0$ respectively.

**B. Insulated Gate Bipolar Transistor (IGBT)**

Similarly, AC-DC power conversion can be obtained by considering Insulated Gate Bipolar Transistor (IGBT) [28]-[30] instead of thyristor. IGBT is a three terminal power device which was designed to turn on and turn off rapidly. An IGBT is turned on by just applying a positive gate voltage and is turned off by removing the gate voltage. The basic principle of operation for an IGBT is depicted in the Fig. 5 with resistive load and the respective input and output voltage with firing pulse is shown in Fig. 6.

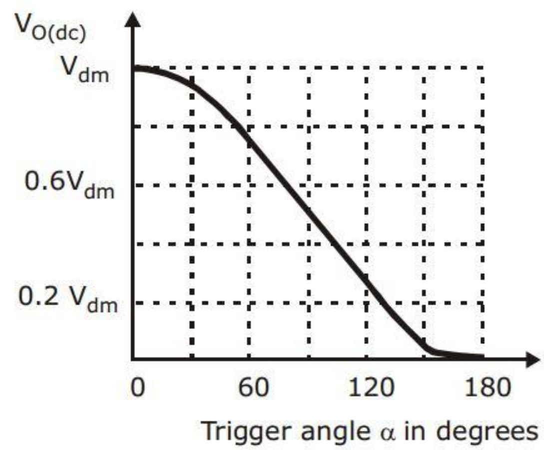


Fig. 4. Variation of output voltage with firing angle, α

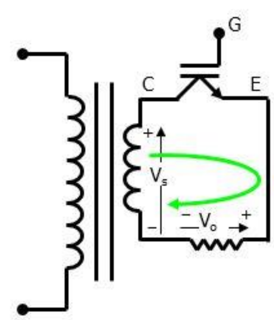


Fig. 5. Single phase half-wave AC-DC converter using IGBT with resistive load

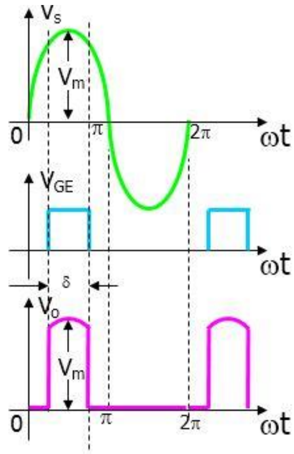


Fig. 6. Input and output voltage wave shape of IGBT based single phase half-wave controlled rectifier with resistive load

The average dc output voltage for this circuit is given by the expression (3),

$$V_{dc} = \frac{V_m}{\pi} \sin\left(\frac{\delta}{2}\right) \tag{3}$$

Here δ is the pulse width of the IGBT.

### C. Total Harmonic Distortion (THD)

Harmonic factor or Total harmonic distortion is a measure of the distortion in the output waveform [31]. The distortion of the normal sine wave by non-linear loads is created by harmonics [32]. Harmonics are related to the fundamental frequency and are defined as whole number multiples of the fundamental frequency. THD of a signal is a measurement of the harmonic distortion present and is defined as the ratio of the sum of all harmonic components of the voltage or current waveform compared against the fundamental component of the voltage or current wave and the expression is (4) [4],

$$THD = \frac{\sqrt{I_2^2 + I_3^2 + \dots\dots\dots\dots + I_N^2}}{I_1} = \frac{\sqrt{\sum_{N=2}^{\infty} I_N^2}}{I_1} \tag{4}$$

Where $I_N$ is the magnitude of the $N_{th}$ order harmonic component of the current.

## III. Firing pulse generation

To generate the firing pulse for Thyristor and IGBT an isolated firing pulse circuit developed using multi-winding transformer [33]. The block diagram and flowchart diagram shown in Fig. 7 & Fig. 8 gives an overall idea about the sequence of the firing pulse generation circuit. The proposed firing pulse circuit consist of zero crossing detector circuit, opto-coupler, micro-controller unit, variable potentiometer to control analog voltage for different firing angle generation.

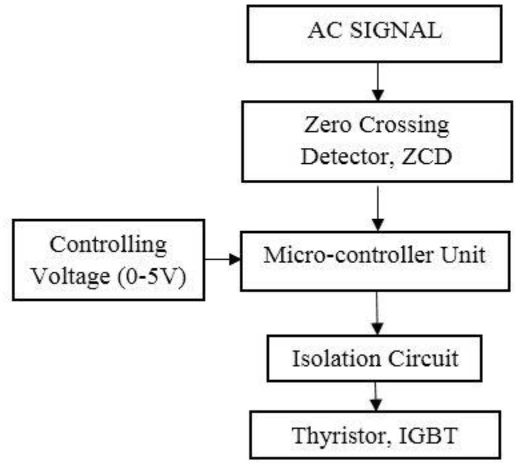


Fig. 7. Block diagram of the firing pulse generation circuit

Integration of all these blocks achieves full controlled converter with advanced performance over other regular techniques. Zero Crossing Detector (ZCD) [34]-[35] module detects the start of positive half cycles or negative half cycles for synchronization of the firing pulses to power supply mains. A potentiometer arrangement is used for varying the control voltage corresponding to different firing angle. The analog voltage received by the microcontroller is converted to digital counts (0-1023) and fed to the inbuilt ADC port within the microcontroller.

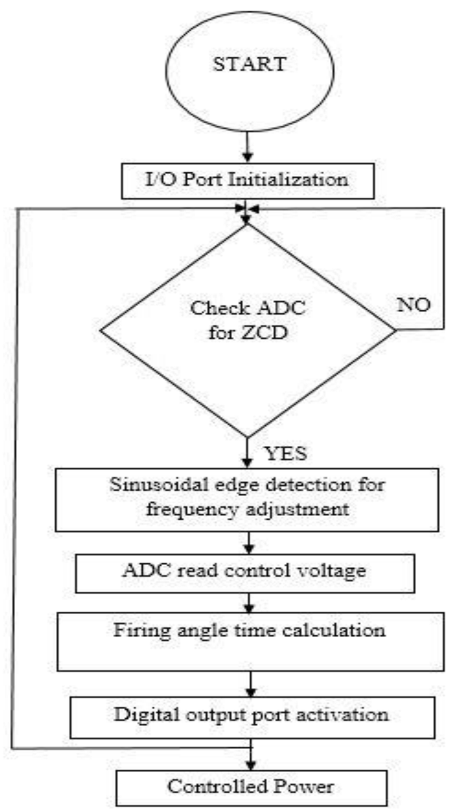


Fig. 8. Flow chart of the firing pulse generation circuit

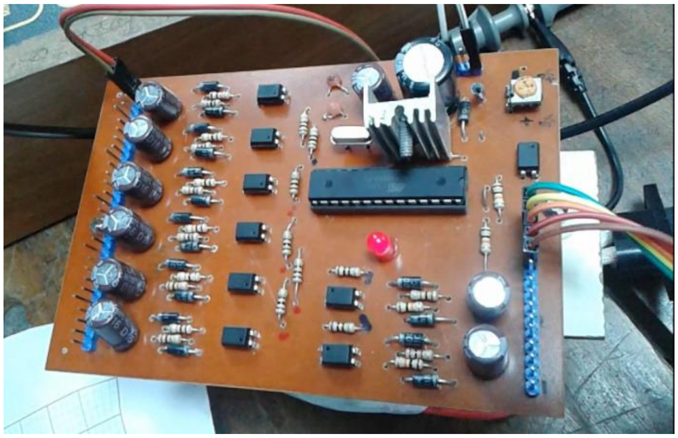

Fig. 9. Photograph of the fabricated circuit

The change in the input analog voltage shall be proportionately converted to the change in digital count. Micro-controller unit accepts analog voltage for the ADC port through the customized potentiometer. At any time when zero crossing (falling edge of square wave) is detected on the AC mains, microcontroller is interrupted and the latest values of ADC is used to determine firing angle with proper mathematical calculations. To control firing pulses from $0^0$-$180^0$ ADC output ranges between 0-1023 counts. The firing pulse generation circuit is fabricated and tested in the lab successfully. A photograph of the firing pulse generation circuit is shown in Fig. 9.

## IV. MATLAB SIMULATIONS

### A. Thyristor Controlled AC-DC Converter

MATLAB/SIMULINK software is used to model a thyristor and IGBT based AC-DC converter circuit with resistive load. The average output voltage ($V_{dc}$) and Total Harmonic Distortion (THD) is obtained by controlling the firing angle of the thyristor. The circuit is simulated for both thyristor and IGBT, under the same output voltage condition. Fig. 10 shows the thyristor based AC-DC converter circuit with resistive load.

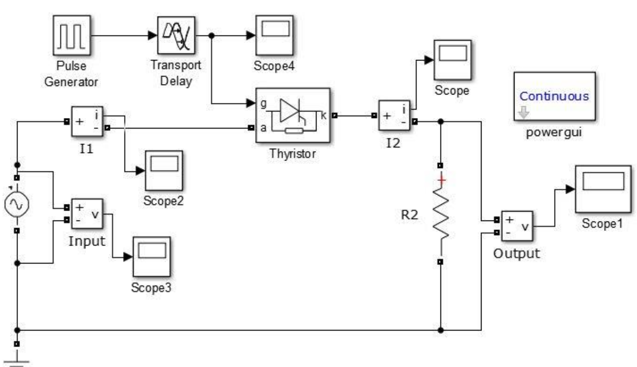


Fig. 10. AC-DC converter circuit using thyristor in MATLAB/SIMULINK

The circuit is tested by considering the following parameters shown in Table I and the firing angle is measured in terms of control voltage (0-5V) and is represented in the following Table II with equivalent time period in milliseconds.

Table I: Parameters used for simulation

| Voltage, Vrms | Frequency, Hz | Peak Voltage, Vm | Load Resistance, R |
|---|---|---|---|
| 220V | 50Hz | 311V | 10 ohm |

Table II: Firing angle relationship with corresponding time period as well as control voltage

| Firing angle, α in degree | $30^0$ | $60^0$ | $90^0$ | $120^0$ | $150^0$ |
|---|---|---|---|---|---|
| Control voltage (0-5V) | 0.833 | 1.67 | 2.50 | 3.33 | 4.17 |
| Time period (T) in millisecond | 1.6667 | 3.3333 | 5 | 6.6667 | 8.333 |

At first thyristor is fired at α= $30^0$, the corresponding output voltage ($V_{dc}$) and Total Harmonic Distortion (THD) is obtained 98V and 55.01% respectively. Thyristor output voltage wave shape and THD is shown in Fig. 11 & Fig. 12 respectively.

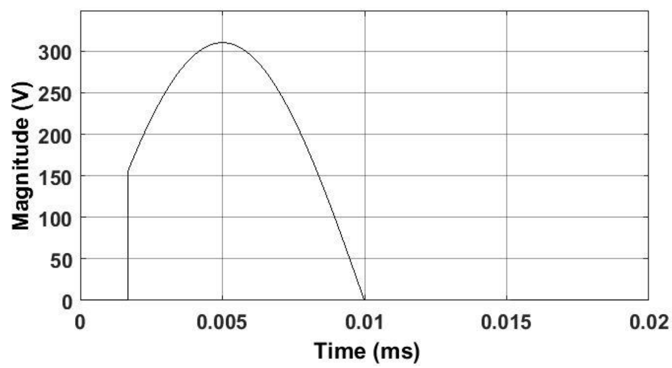


Fig. 11. Simulated Output voltage of thyristor fired at $30^0$

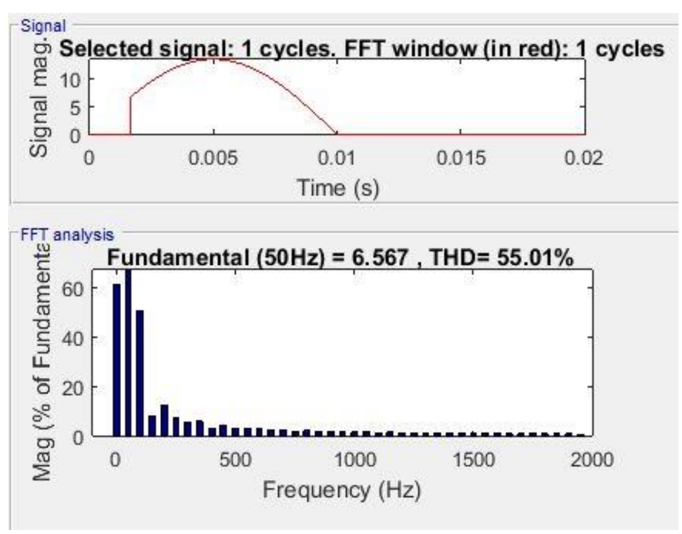

Fig. 12. Simulated THD of thyristor fired at $30^0$

Next thyristor is fired at $\alpha = 60^0$, the corresponding output voltage ($V_{dc}$) and Total Harmonic Distortion (THD) is obtained 78.78V and 80.02% respectively. Thyristor output voltage wave shape and THD is shown in Fig. 13 & Fig. 14 respectively.

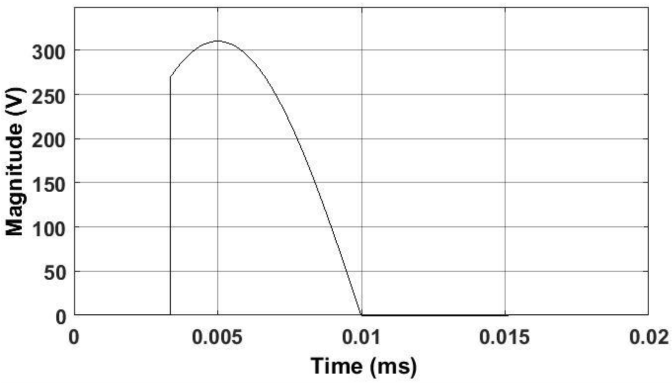


Fig. 13. Output voltage of thyristor fired at $60^0$

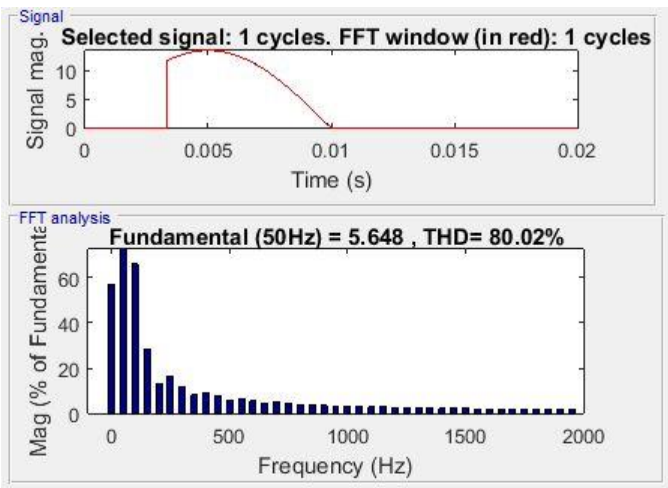


Fig. 14. THD of thyristor fired at $60^0$

Similarly thyristor is fired at $\alpha = 90^0$, the corresponding output voltage ($V_{dc}$) and Total Harmonic Distortion (THD) is obtained 52.52V and 113.31% respectively. Thyristor output voltage wave shape and THD is shown in Fig. 15 & Fig. 16 respectively.

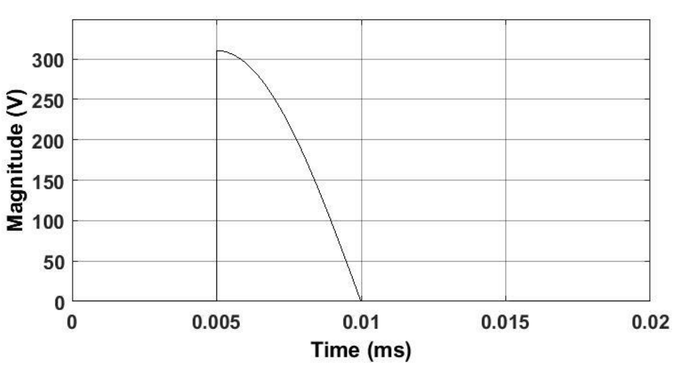


Fig. 15. Output voltage of thyristor fired at $90^0$

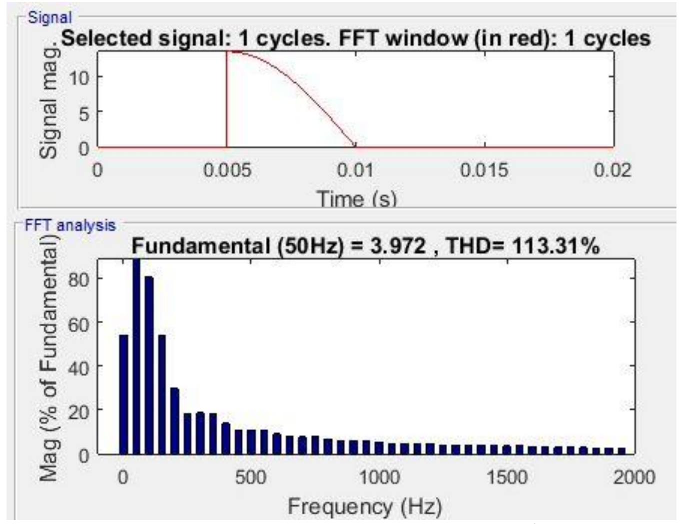


Fig. 16. THD of thyristor fired at $90^0$

Again thyristor is fired at $\alpha = 120^0$, the corresponding output voltage ($V_{dc}$) and Total Harmonic Distortion (THD) is obtained 26.26V and 162.21% respectively. Thyristor output voltage wave shape and THD is shown in Fig. 17 & Fig. 18 respectively.

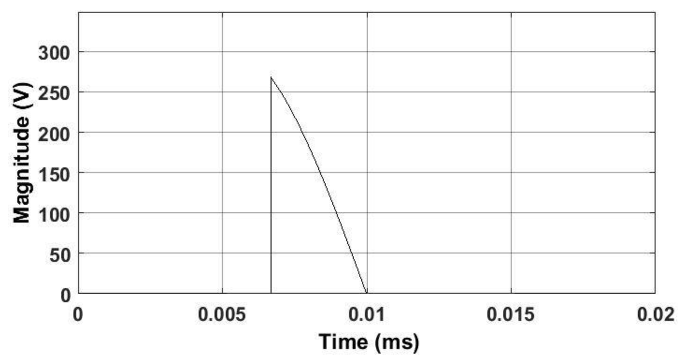


Fig. 17. Output voltage of thyristor fired at $120^0$

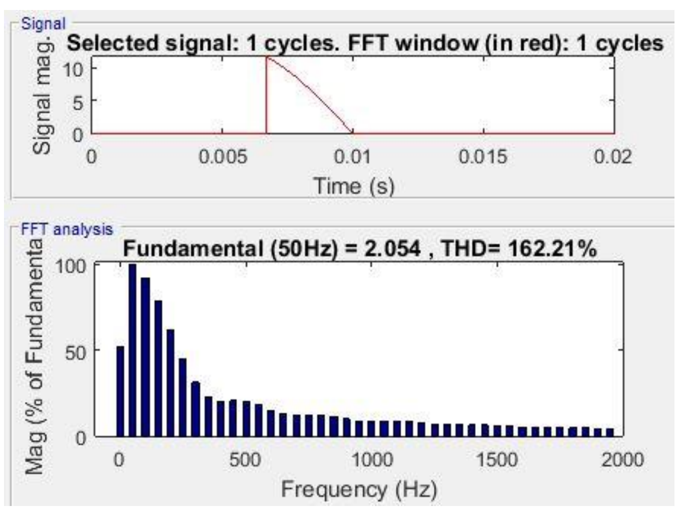


Fig. 18. THD of thyristor fired at $120^0$

At last thyristor is fired at $\alpha = 150^0$, the corresponding output voltage (Vdc) and Total Harmonic Distortion (THD) is obtained 7.04V and 266.79% respectively. Thyristor output voltage wave shape and THD is shown in Fig. 19 & Fig. 20 respectively.

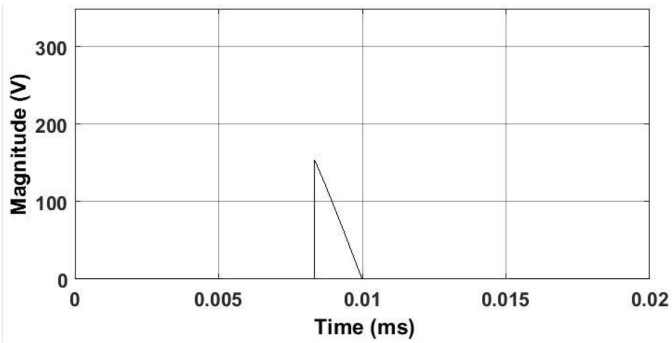


Fig. 19. Output voltage of thyristor fired at $150^0$

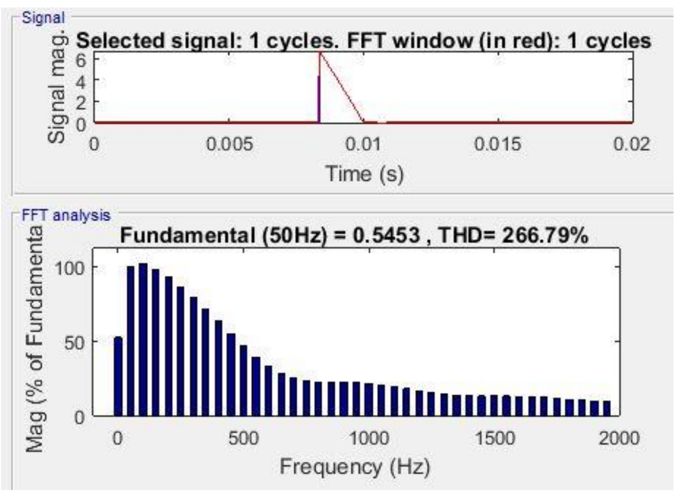


Fig. 20. THD of thyristor fired at $150^0$

## B. IGBT Controlled AC-DC Converter

An IGBT based AC-DC converter also simulated as well as in MATLAB/SIMULINK for resistive load only, as shown in Fig. 21. The parameters are taken as same as in thyristor in Table I.

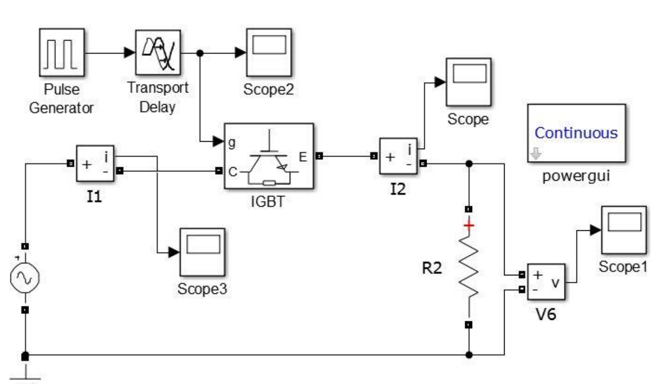


Fig. 21. AC-DC converter circuit using IGBT in MATLAB/SIMULINK

The following Table III represents the firing angle of thyristor with corresponding output voltage and pulse width of IGBT for various condition. For the initial simulation pulse width of IGBT is considered $\delta = 137.82^0$ which corresponds to the firing angle of thyristor, $\alpha = 30^0$ for the same output voltage, Vdc= 98V. For this pulse width Total Harmonic Distortion (THD) obtained from simulation is 55.38%. The output voltage wave shape and THD is shown in Fig. 22 & Fig. 23 respectively.

Table III: IGBT pulse width and output voltage with corresponding thyristor firing angle

| Thyristor firing angle, α in degree | Average output voltage, $V_{dc}$ in volt | IGBT pulse width, δ in degree |
|---|---|---|
| $30^0$ | 98.00 | $137.82^0$ |
| $60^0$ | 78.78 | $97.18^0$ |
| $90^0$ | 52.52 | $59.99^0$ |
| $120^0$ | 26.26 | $28.96^0$ |
| $150^0$ | 7.03 | $7.68^0$ |

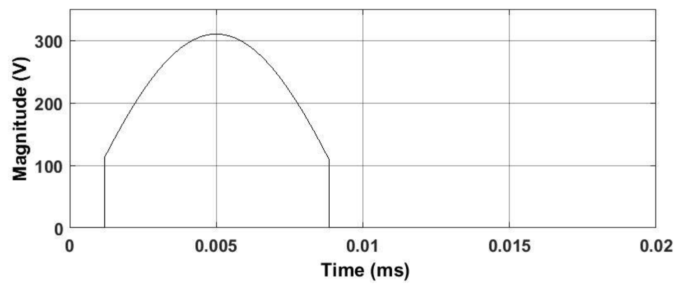


Fig. 22. Output voltage wave shape of IGBT for pulse width $\delta = 137.82^0$

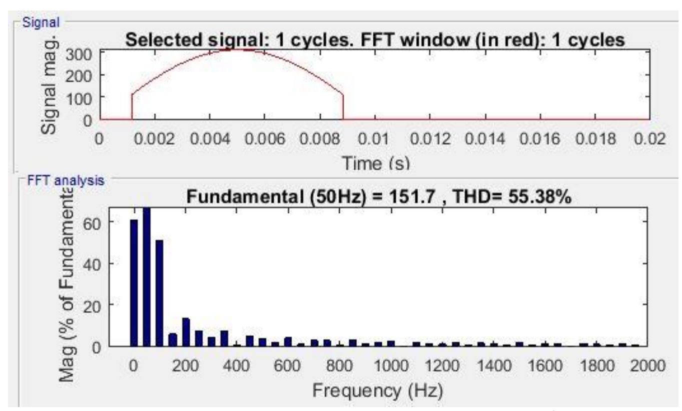


Fig. 23. THD for pulse width $\delta = 137.82^0$

For the next simulation pulse width of IGBT is considered $\delta = 97.18^0$ which corresponds to the firing angle of thyristor, $\alpha = 60^0$ for the same output voltage, Vdc= 78.78V. For this pulse width Total Harmonic Distortion (THD) obtained from simulation is 84.59%. The output voltage wave shape and THD is shown in Fig. 24 & Fig. 25 respectively.

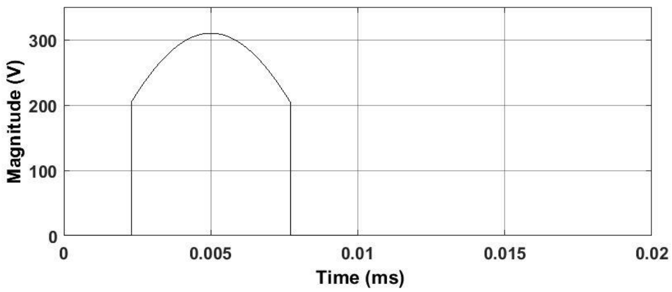


Fig. 24. Output voltage wave shape of IGBT for Pulse width $\delta=97.18^0$

Again for the simulation pulse width of IGBT is considered $\delta= 59.99^0$ which corresponds to the firing angle of thyristor, $\alpha= 90^0$ for the same output voltage, $V_{dc}$= 52.52V. For this pulse width Total Harmonic Distortion (THD) obtained from simulation is 131.41%. The output voltage wave shape and THD is shown in Fig. 26 & Fig. 27 respectively.

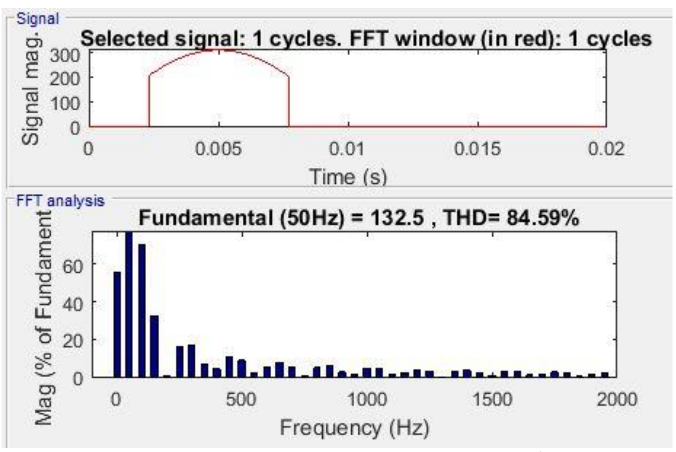


Fig. 25. THD for pulse width $\delta=97.18^0$

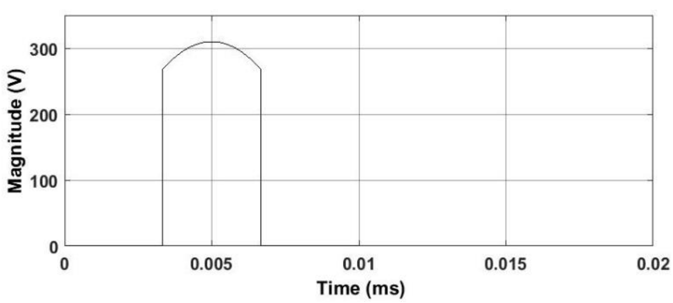


Fig. 26. Output voltage wave shape of IGBT for Pulse width $\delta=59.99^0$

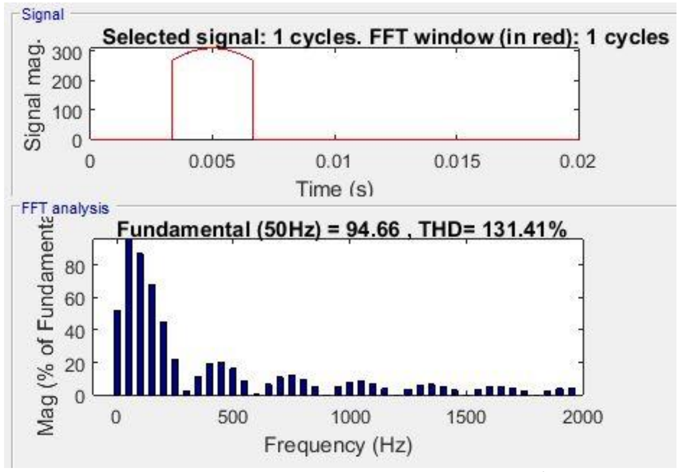


Fig. 27. THD for pulse width $\delta=59.99^0$

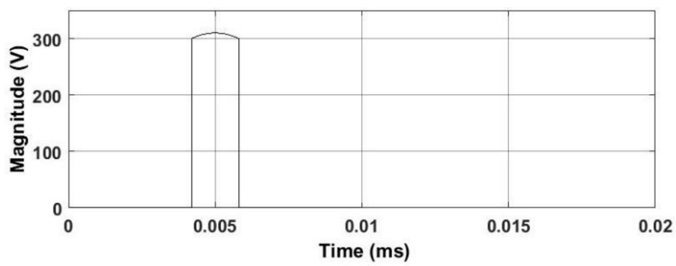


Fig. 28. Output voltage wave shape of IGBT for Pulse width $\delta=28.96^0$

Similarly for the simulation pulse width of IGBT is considered $\delta= 28.96^0$ which corresponds to the firing angle of thyristor, $\alpha=120^0$ for the same output voltage, $V_{dc}$= 26.26V. For this pulse width Total Harmonic Distortion (THD) obtained from simulation is 219.31%. The output voltage wave shape and THD is shown in Fig. 28 & Fig. 29 respectively.

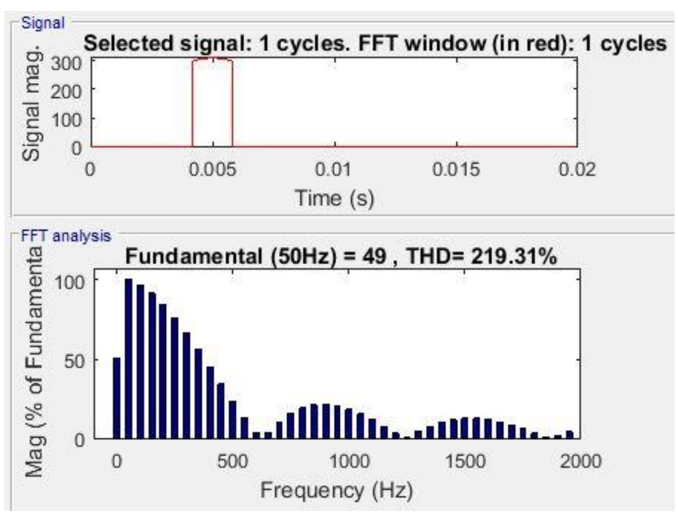


Fig. 29. THD for pulse width $\delta=28.96^0$

Lastly for the simulation pulse width of IGBT is considered $\delta= 7.68^0$ which corresponds to the firing angle of thyristor, $\alpha= 150^0$ for the same output voltage, $V_{dc}$= 7.03V. For this pulse width Total Harmonic Distortion (THD) obtained from simulation is

465.41%. The output voltage wave shape and THD is shown in Fig. 30 & Fig. 31 respectively.

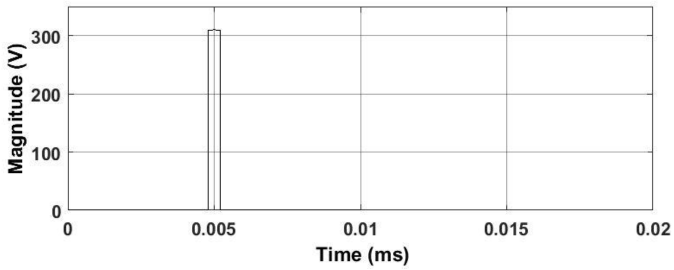


Fig. 30. Output voltage wave shape of IGBT for Pulse width $\delta$=7.68$^0$

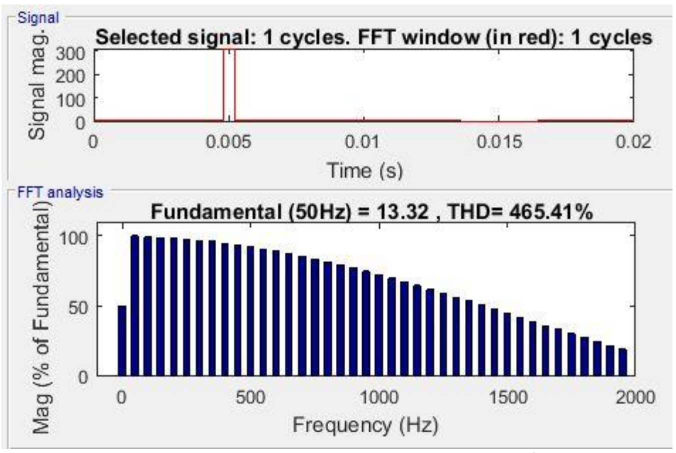


Fig. 31. THD for pulse width $\delta$=7.68$^0$

It is observed that percentage of THD increased along with the increase of firing angle of thyristor as well as IGBT. A summary of the results of THD for thyristor and IGBT is represented in Table IV.

Table IV: Summary of THD for Thyristor and IGBT

| Thyristor | | | IGBT | |
|---|---|---|---|---|
| Firing angle, α in degree | Average output voltage ($V_{dc}$) in Volt | THD (%) | Pulse width, $\delta$ in degree | THD (%) |
| 30$^0$ | 98.00 | 55.00 | 137.82$^0$ | 55.38 |
| 60$^0$ | 78.78 | 79.35 | 97.18$^0$ | 84.59 |
| 90$^0$ | 52.52 | 111.63 | 59.99$^0$ | 131.41 |
| 120$^0$ | 26.26 | 158.79 | 28.96$^0$ | 219.31 |
| 150$^0$ | 7.04 | 252.97 | 7.68$^0$ | 465.41 |

## V. Experimental Results

### A. Silicon Controlled AC-DC Converter (SCR or Rectifier)

The firing pulse circuit is developed in the laboratory to verify the simulation results with experimental observation. A 12V prototype circuit is implemented and tested with a 25W incandescent lamp as a load in the laboratory. Parameters used in the test are given in Table V.

### B. Digital Oscilloscope Rigol DS1000Z Series

To analyze the Total Harmonic Distortion (THD) and output voltage wave shape a special type of 4 channel digital oscilloscope is shown in Fig. 32 took in consideration in this research. The main features of DS1054Z is presented in Table VI.

Table V: Parameters used for laboratory experiment

| Voltage, Vrms | Frequency, Hz | Peak Voltage, Vm | Load Resistor, R | Load Power, P |
|---|---|---|---|---|
| 12V | 50Hz | 16.6V | 23 ohm | 25W |

Table VI: DS1054Z function parameters

| | |
|---|---|
| Waveform Operation | A+B, A-B, A x B, A/B, FFT |
| FFT Window Function | Rectangle, Hanning, Triangle, Blackman, Flat top |
| FFT Mode | Trace, Memory |
| FFT Display | Half, Full |
| FFT Vertical Scale | dB/dBm, Vrms |
| Standard Ports | USB Host, USB Device, LAN |
| Sample Rate | 200 MSa/s |
| Max. Frequency | 25MHz |
| Number of channel | 4 nos |


Fig. 32. Front view of DS1054Z oscilloscope

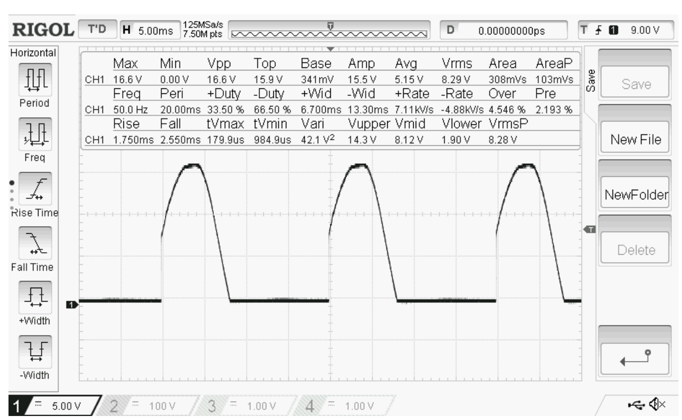

Fig. 33. Output voltage wave shape of thyristor fired at $30^0$ captured by oscilloscope

At first the thyristor firing pulse considered as $\alpha = 30^0$. For this firing pulse observed data found in oscilloscope is Vdc =5.17V, $V_{rms}$ = 8.28V and $V_m$ =16.6V. The output voltage wave shape and THD is shown in Fig. 33 and Fig. 34.

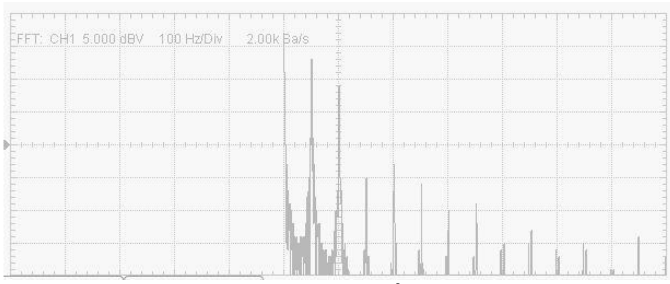


Fig. 34. THD of thyristor fired at $30^0$ captured by oscilloscope

Next the thyristor firing pulse considered as $\alpha = 60^0$. For this firing pulse observed data found in oscilloscope is Vdc =4.50V, $V_{rms}$ = 7.87V and $V_m$ =16.6V. The output voltage wave shape and THD is shown in Fig. 35 and Fig. 36.

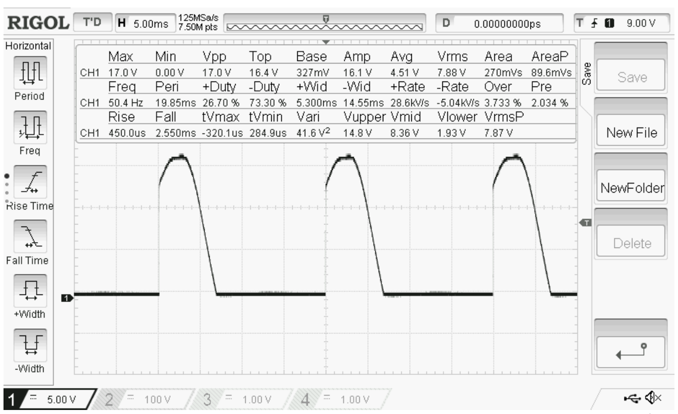


Fig. 35. Output voltage wave shape of thyristor fired at $60^0$ captured by oscilloscope

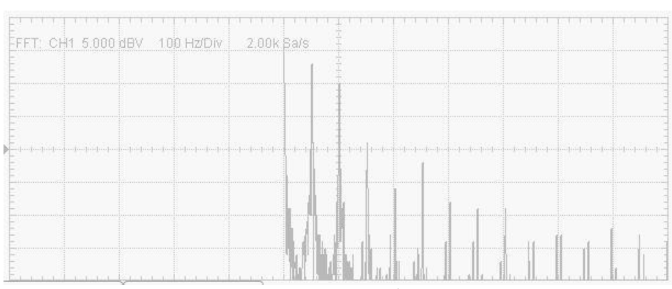


Fig. 36. THD of thyristor fired at $60^0$ captured by oscilloscope

Again the thyristor firing pulse considered as $\alpha = 90^0$. For this firing pulse observed data found in oscilloscope is Vdc =3.62V, $V_{rms}$ = 6.94V and $V_m$ =16.6V. The output voltage wave shape and THD is shown in Fig. 37 and Fig. 38.

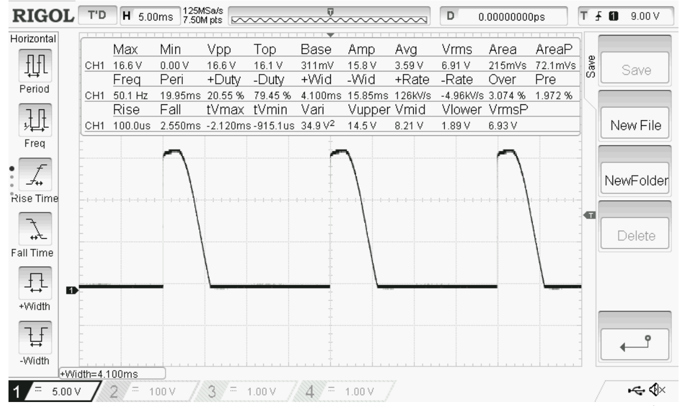


Fig. 37. Output voltage wave shape of thyristor fired at $90^0$ captured by oscilloscope

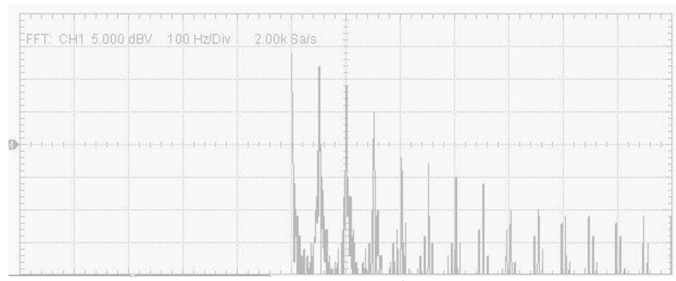


Fig. 38. THD of thyristor fired at $90^0$ captured by oscilloscope

Similarly the thyristor firing pulse considered as $\alpha = 120^0$. For this firing pulse observed data found in oscilloscope is Vdc =3.09V, $V_{rms}$ = 6.24V and $V_m$ =16.6V. The output voltage wave shape and THD is shown in Fig. 39 and Fig. 40.

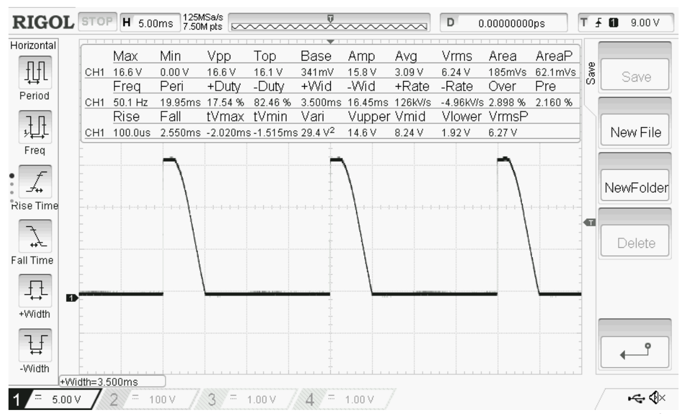


Fig. 39. Output voltage wave shape of thyristor fired at $120^0$ captured by oscilloscope

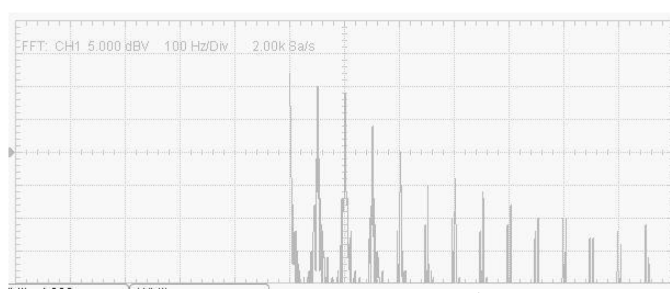


Fig. 40. THD of thyristor fired at $120^0$ captured by oscilloscope

Finally the thyristor firing pulse considered as α= $150^0$. For this firing pulse observed data found in oscilloscope is Vdc =1.51V, $V_{rms}$ = 3.57V and $V_m$ =16.6V. The output voltage wave shape and THD is shown in Fig. 41 and Fig. 42.

Fig. 41. Output voltage wave shape of thyristor fired at $150^0$ captured by oscilloscope

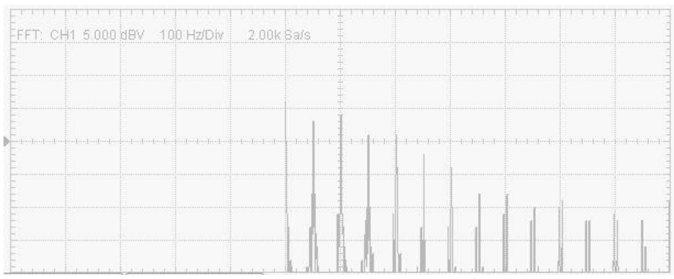

Fig. 42. THD of thyristor fired at $150^0$ captured by oscilloscope

## B. IGBT Controlled AC-DC Converter

Similarly for IGBT experimental work done by taking all the parameters are equal as in thyristor. Pulse width of IGBT found in oscilloscope converted from millisecond to degree. THD calculation using the oscilloscope DS1054Z is not possible.

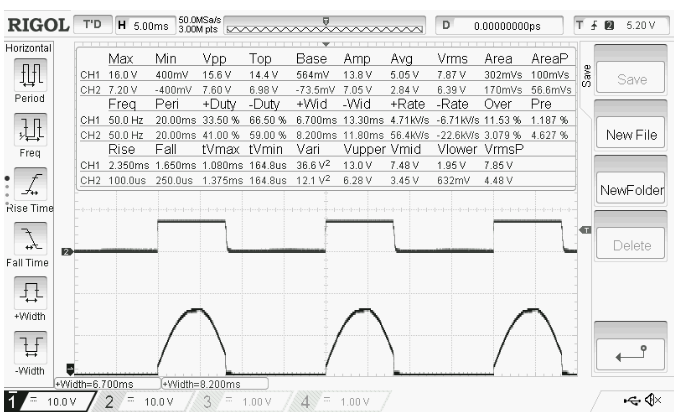

Fig. 43. Output voltage wave shape of IGBT based converter for pulse width δ= $147.6^0$

For this reason, we have consider MATLAB simulation for the THD presented in Table VI. At first pulse width of IGBT is considered δ= $147.6^0$ which corresponds to the firing angle of thyristor, α= $30^0$ for the same output voltage, Vdc= 5.03V. For this pulse width Total Harmonic Distortion (THD) obtained from simulation is 51.87%. The output voltage wave shape and THD is shown in Fig. 43 & Fig. 44 respectively.

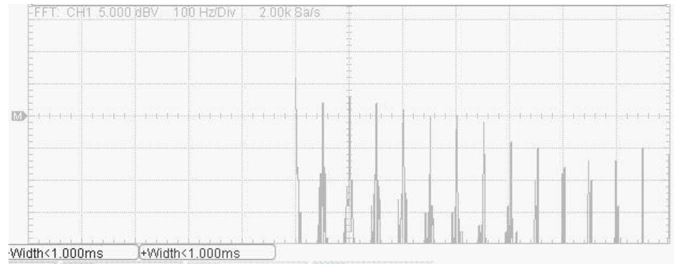

Fig. 44. THD for pulse width δ= $147.6^0$

Next pulse width of IGBT is considered δ= $113.4^0$ which corresponds to the firing angle of thyristor, α= $60^0$ for the same output voltage, Vdc= 4.50V. For this pulse width Total Harmonic Distortion (THD) obtained from simulation is 70.70%. The output voltage wave shape and THD is shown in Fig. 45 & Fig. 46 respectively.

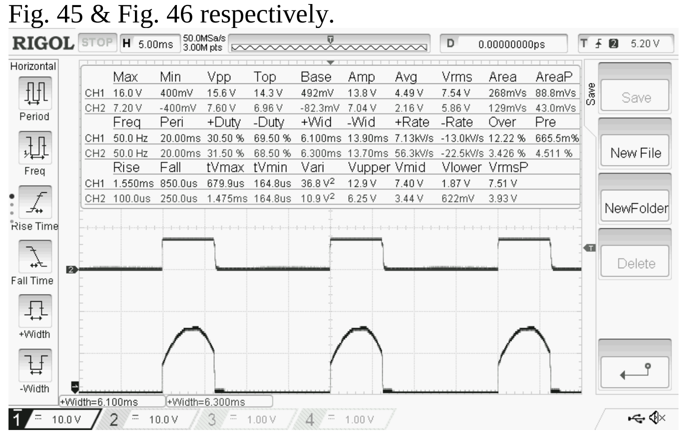

Fig. 45. Output voltage wave shape of IGBT for pulse width δ= $113.4^0$

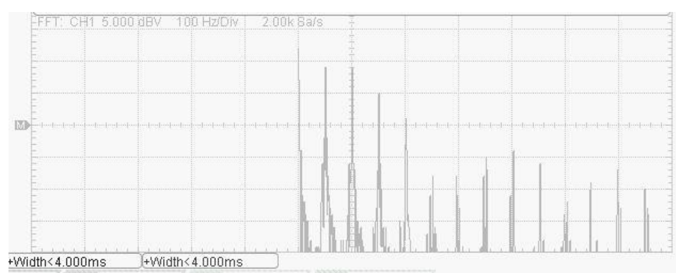

Fig. 46. THD for pulse width δ= $113.4^0$

Similarly pulse width of IGBT is considered δ= $82.8^0$ which corresponds to the firing angle of thyristor, α= $90^0$ for the same output voltage, Vdc= 3.62V. For this pulse width Total Harmonic Distortion (THD) obtained from simulation is 98.66%. The output voltage wave shape and THD is shown in Fig. 47 & Fig. 48 respectively.

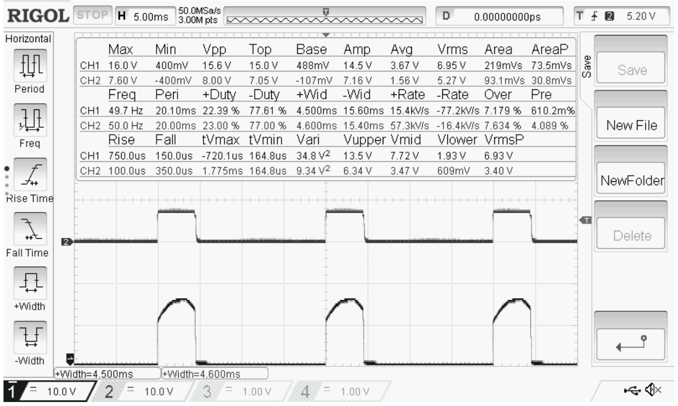


Fig. 47. Output voltage wave shape of IGBT based converter for pulse width δ= 82.8$^0$

Again pulse width of IGBT is considered δ= 64.8$^0$ which corresponds to the firing angle of thyristor, α= 120$^0$ for the same output voltage, $V_{dc}$= 3.09V. For this pulse width Total Harmonic Distortion (THD) obtained from simulation is 122.71%. The output voltage wave shape and THD is shown in Fig. 49 & Fig. 50 respectively.

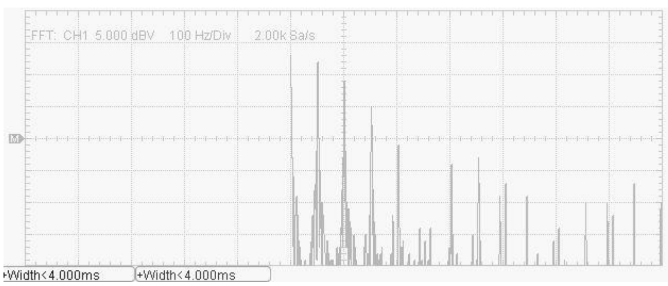


Fig. 48. THD for pulse width δ= 82.8$^0$

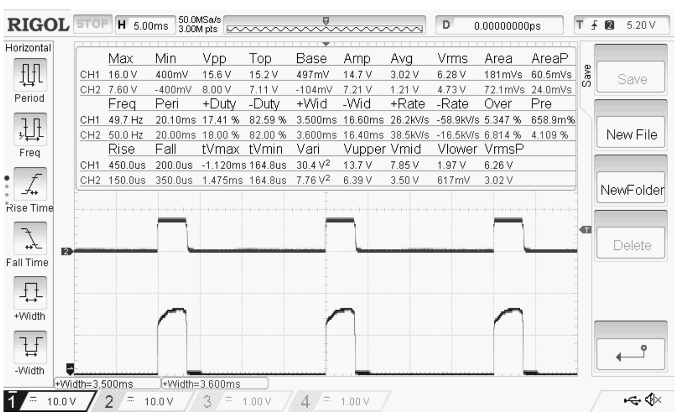


Fig. 49. Output voltage wave shape of IGBT based converter for pulse width δ= 64.8$^0$

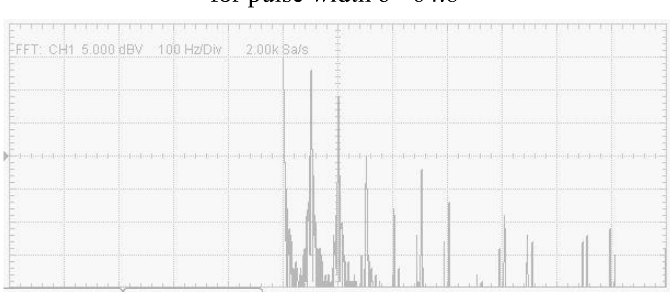


Fig. 50. THD for pulse width δ= 64.8$^0$

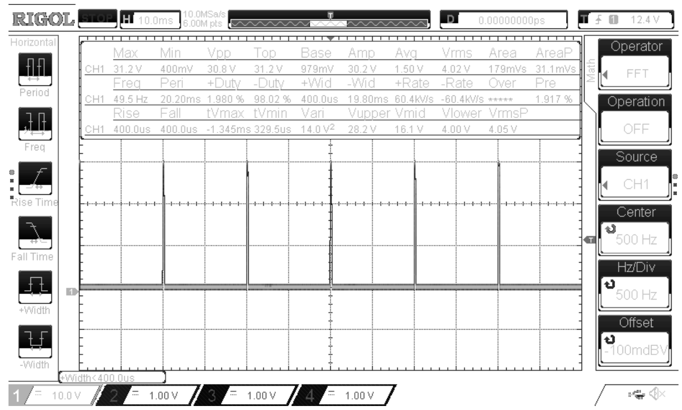


Fig. 51. Output voltage wave shape of IGBT based converter for pulse width δ= 27.18$^0$

Finally pulse width of IGBT is considered δ= 27.18$^0$ which corresponds to the firing angle of thyristor, α= 150$^0$ for the same output voltage, $V_{dc}$= 1.51V. For this pulse width Total Harmonic Distortion (THD) obtained from simulation is 223.27%. The output voltage wave shape and THD is shown in Fig. 51 & Fig. 52 respectively.

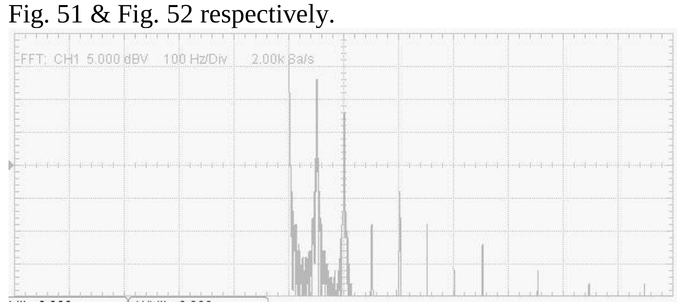


Fig. 52. THD for pulse width δ= 27.18$^0$

A summary of the experimental results of THD for thyristor and IGBT is represented in Table VII.

Table VII: Summary of THD for Thyristor and IGBT

| Thyristor | | | IGBT | |
|---|---|---|---|---|
| Firing angle, α in degree | Average Output Voltage ($V_{dc}$) in Volt | THD (%) | Pulse Width, $\delta$ in degree | THD (%) |
| 30$^0$ | 5.03 | 56.21 | 147.6$^0$ | 60.87 |
| 60$^0$ | 4.50 | 80.90 | 113.4$^0$ | 95.70 |
| 90$^0$ | 3.62 | 115.81 | 82.8$^0$ | 122.66 |
| 120$^0$ | 3.09 | 166.96 | 64.8$^0$ | 210.71 |
| 150$^0$ | 1.51 | 283.46 | 27.18$^0$ | 305.27 |

## VI. Conclusion

In this paper, Thyristor and IGBT based AC-DC power converter has been simulated and tested successfully with resistive load. Experimental findings found symmetrical with simulation result in both cases and THD of IGBT found higher than thyristor for the equal output voltage ($V_{dc}$). It is observed that IGBT based power converter introduces more harmonics in the system, in spite of more symmetrical output voltage wave shape. A micro-controller based control circuit is designed and implemented to generate the firing pulse for both thyristor and IGBT. The control circuit is developed using a multi-winding transformer for the generation of isolated firing pulse.

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